RTD Park-n-Ride Niwot Road and 63rd Street CO 119 Safety and Mobility Improvement

PRELIMINARY DRAINAGE REPORT

August 4, 2022

Prepared by:



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I. PROJECT DESCRIPTION AND LOCATION

The proposed CO 119 Safety and Mobility Improvements project is a joint effort project between Colorado Department of Transportation (CDOT) and Regional Transportation District (RTD). The main purpose of the proposed CO 119 project is to improve and update the existing state highway corridor and make traveling safer, faster, and reliable for all modes of available transportation.

The proposed CO 119 project improvements will include queue bypass lanes, bus rapid transit (BRT) stations, RTD Park-n-Rides (P-n-R), and many other physical and signal improvements on the corridor. A new RTD P-n-R facility will be located at the intersection of CO 119 and 63rd Street and an existing smaller RTD P-n-R at the intersection of CO 119 and Niwot Road will be replaced with a larger P-n-R as part of this project. The two proposed RTD P-n-Rs are located within the CDOT Right-of-Way (ROW) in Boulder County, Colorado. The 63rd Street and Niwot Road P-n-R locations are shown on the Location Map (Figure 1, Appendix A).

The purpose of this drainage report is to document the preliminary drainage analysis and design for the two proposed RTD P-n-Rs included in the CO 119 project. For discussions and drainage information on the other proposed CO 119 highway improvements, please refer to the Preliminary Drainage Report for CO 119 Safety and Mobility Improvement Project, dated August 2022, prepared by Muller Engineering Company (Reference 4).

A. Niwot Road P-n-R

The proposed RTD Niwot Road P-n-R is located within the CDOT ROW/highway median area between the CO 119 southbound (SB) and northbound (NB) lanes, immediately north of Niwot Road. Currently, a small paved RTD P-n-R is located at this location. Outside of the footprint of the existing P-n-R and roadways, the site is undeveloped and mainly consists of grassy vegetation. An existing earthen embankment separates the project site from an existing CDOT water quality basin which is located north of the P-n-R site. There is an existing 18" RCP under the earthen embankment that drains the project site into the CDOT water quality basin.

1. Major Drainageway

There is no major drainageway that crosses the proposed Niwot Road P-n-R project site. The surface runoff from the project site and adjacent roadways currently drains north into an existing CDOT water quality basin which is located directly north of the project site within the CDOT ROW. Also, there is an existing 18inch RCP culvert under Niwot Road near CO 119 NB lanes which conveys flows north from the CO 119 median area (south of Niwot Road) through the project site to the existing CDOT water quality basin.

2. Natural Resources Conservation Service (NRCS) Soils Classification

The predominant NRCS hydrologic soil classification for the proposed Niwot Road P-n-R site and the surrounding area is Type C. Type C soil has a slow rate of storm water infiltration when saturated. Detailed NRCS map and soil information are included in Appendix C.

3. Irrigation Facilities

The Niwot Road P-n-R project site does not contain any existing ditches or canals that convey irrigation flows.

4. **FEMA** Floodplain

As shown on the FEMA Flood Insurance Rate Map (FIRM) Panel 410 of 615 (Map Number 08013C0410J), revised December 18, 2012, for Boulder County, Colorado and Incorporated Areas, the Niwot P-n-R project site is not located within the FEMA Special Flood Hazard Areas (see FEMA Firmette in Appendix B). The proposed P-n-R site is currently designated as unshaded Zone X, area of minimal flood hazard.

B. 63rd Street P-n-R

The proposed 63rd Street P-n-R is located within the CDOT ROW/highway median area between the CO 119 southbound (SB) and northbound (NB) lanes, immediately west of 63rd street. Currently, the site is undeveloped outside of the footprint of the existing roadways and mainly consists of grassy vegetation.

1. Major Drainageway

A tributary creek known as Little Dry Creek, which connects to Dry Creek North at a downstream location, dissects the proposed 63rd Street P-n-R project site. Little Dry Creek conveys runoff from the offsite drainage basin area, north and west of the SB CO 119 and flow releases from the Boulder Reservoir through the proposed RTD P-n-R site. There is an existing 10'x6' concrete box culvert (CBC) under both SB and NB CO 119 elevated roadway embankments. The surface runoff from the proposed P-n-R project site currently sheet flows into Little Dry Creek, upstream of the CO 119 NB CBC crossing.

In order to build the proposed 63rd Street P-n-R, the existing Little Dry Creek between the NB and SB CO 119 will be filled in and replaced with 10'x6' CBCs which will connect with the existing 10'x6' CBCs under NB and SB CO 119. For more detailed discussions regarding the hydrologic and hydraulic analyses and design of the existing and proposed 10'x6' CBCs, please refer to the Preliminary Drainage Report for CO 119 Safety and Mobility Improvement Project, dated August 2022, prepared by Muller Engineering Company (Reference 4).

2. Natural Resources Conservation Service (NRCS) Soils Classification

The predominant NRCS hydrologic soil classification for the 63rd Street P-n-R project site and the surrounding area is Type D. Type D soil has a very slow rate of storm water infiltration when saturated. Detailed NRCS map and soil information are included in Appendix C.

3. Irrigation Facilities

The 63rd Street P-n-R project site does not contain any existing ditches or canals that convey irrigation flows.

4. **FEMA Floodplain**

As shown on the FEMA Flood Insurance Rate Map (FIRM) Panel 404 of 615 (Map Number 08013C0404J), revised December 18, 2012, for Boulder County, Colorado and Incorporated Areas, the RTD P-n-R project site is not located within the FEMA Special Flood Hazard Areas (see FEMA Firmette in Appendix B). The proposed P-n-R site is currently designated as unshaded Zone X, area of minimal flood hazard.

II. DRAINAGE DESIGN CRITERIA

A. Hydrology Criteria

1. Design Rainfall

The rainfall depths used for the two proposed RTD P-n-R project sites were obtained from NOAA Atlas 14 Precipitation Frequency Atlas of the United States, Volume 8, Version 2 (Reference 1).

2. Runoff Calculation Method

Rational Method was used to estimate peak flow rates for all existing and proposed conditions drainage basins since they are less than 90 areas in size. Mile High Flood District's (MHFD) spreadsheet program, UD-Rational, Version 2.0 was used to perform the Rational Method hydrologic calculations.

3. Design Storm Recurrence Intervals

The following minor and major design storm events are used for the proposed P-n-R sites based on the guidelines provided in the Boulder County Storm Drainage Criteria Manual (Reference 2).

- Minor Storm: 5-year
- Major Storm: 100-year

B. Hydraulics Criteria

The proposed storm drain inlets and pipes are designed to convey the computed 100-year peak flow rates for the proposed P-n-R site developed conditions. The design capacities of the proposed storm drain inlets were analyzed utilizing the MHFD's spreadsheet program MHFD-Inlet v5.01. Per RTD's P-n-R design criteria, all proposed storm drain inlets are designed to capture the computed 100-year peak flows with maximum ponding depths of 6 inches or less.

The proposed storm drain pipes are initially sized based on normal depth calculations using Bentley FlowMaster V8i for the Preliminary Drainage Report. The MHFD's UDSewer program will be used to check the HGL/EGL elevations of the proposed storm drain pipe systems for the Final Drainage Report.

Based on the water quality and detention requirements for new developments outlined in the Boulder County Storm Drainage Criteria Manual (Reference 2), a full-spectrum detention basin (DB) will be provided at both proposed RTD P-n-R locations. The MHFD's detention basin design workbook, MHFD-Detention, Version 4.05 was used to perform preliminary analyses of the proposed full-spectrum detention basins.

C. Waivers from Criteria

None identified at the current stage of P-n-R drainage system design.

III. EXISTING DRAINAGE CONDITIONS

A. Niwot Road P-n-R

The existing conditions drainage basin boundaries have been delineated based on the recent survey of the proposed P-n-R site as shown on Figure 2 (Appendix D). Surface runoff from the delineated drainage basin NW-EX1 concentrates at the low-lying area adjacent to the earthen embankment (CP N1) and flow north through an existing 18-inch RCP culvert into the CDOT water quality basin. There is no existing formal detention basin within NW-EX1.

Currently, a small paved RTD P-n-R facility is located within basin NW-EX1. Surface runoffs from the existing paved Niwot Road and CO 119 NB and SB lanes within basin NW-EX1 sheet flow to CP N1. Outside of the footprint of the existing P-n-R and roadways, the site is undeveloped and mainly consists of grassy vegetation. The computed existing conditions 100-year peak flow rate from basin NW-EX1 is 15.5 cfs.

There is an existing 18-inch RCP culvert under Niwot Road near CO 119 NB lanes which conveys flows north from the CO 119 median area (south of Niwot Road) through basin NW-EX1 to the existing CDOT water quality basin. The approximate flow conveyance capacity of the existing 18-inch RCP culvert under Niwot Road was estimated (13.3 cfs) using a flowing-full pipe culvert normal depth calculation (Appendix G).

B. 63rd Street P-n-R

The existing conditions drainage basin boundaries have been delineated based on the recent survey of the proposed P-n-R site as shown on Figure 4 (Appendix D). Surface runoff from the delineated drainage basin 63-EX1 flows into Little Dry Creek and concentrates near the inlet of the existing 10'x6' CBC under CO 119 NB lanes (CP 1). Surface runoffs from the existing paved 63rd Street and CO 119 NB and SB lanes within the basin 63-EX1 sheet flow to CP 1. Outside of the footprint of the existing paved roadways and trail, the site is undeveloped and mainly consists of grassy vegetation. The computed existing conditions 100-year peak flow rate from basin 63-EX1 is 17.3 cfs. An offsite drainage basin (P172C) which is comprised of CO 119 median area between NB ad SB lanes, south of the proposed P-n-R site, also flows into Little Dry Creek near CP 1. The computed 100-year peak flow rate from basin P172C is 11.9 cfs (Reference 4).

Little Dry Creek conveys runoff from the offsite drainage basin area, north and west of the SB CO 119 and flow releases from the Boulder Reservoir through the proposed RTD P-n-R site. There is an existing 10'x6' concrete box culvert (CBC) under both SB and NB CO 119 elevated roadway embankments. The flows in Little Dry Creek combine with surface runoffs from basins 63-EX1 and P172C and flow through the existing 10'x6' CBC under CO 119 and 63rd Street in a southeasterly direction.

In order to build the proposed 63rd Street P-n-R, the existing Little Dry Creek between the NB and SB CO 119 will be filled in and replaced with 10'x6' CBCs which will connect with the existing 10'x6' CBCs under NB and SB CO 119. For detailed discussions and analysis/design information on the existing and proposed 10'x6' CBCs and basin P172C, please refer to the Preliminary Drainage Report for CO 119 Safety and Mobility Improvement Project, dated August 2022, prepared by Muller Engineering Company (Reference 4).

IV. PROPOSED DRAINAGE CONDITIONS

A. Niwot Road P-n-R

1. Proposed Drainage Basins

The proposed conditions drainage subbasin boundaries (NW-PR1 through NW-PR8) have been delineated to reflect the proposed site improvement conditions (see Figure 3, Appendix D). In general, the 100-year flows from the proposed RTD P-n-R improvements (NW-PR1 through NW-PR5) including bus ramps, station platforms, and P-n-R parking lot will be captured and conveyed to the proposed onsite full spectrum detention basin (DB). However, some portions of Niwot Road and CO 119 that surface drain into the proposed bus ramps will also be captured and conveyed to the proposed onsite DB. Surface runoffs from the remaining Niwot Road and CO 119 NB and SB lanes (NW-PR6 through NW-PR8) will flow directly into the existing CDOT water quality basin.

The proposed adjacent paved bike trail area (approximately 5960 sf) will drain south to new sump pumps at the low point of the Niwot Road trail underpass. This bike trail area is excluded from RTD's Pn-R proposed conditions hydrologic analysis since the trail area will not drain into RTD's onsite storm drainage and detention systems and the location of the sump pump discharge outfall has not been identified at the current stage of the trail design.

2. Storm Drain Improvements

The proposed P-n-R onsite storm drain systems are sized to capture and convey the computed 100-year peak flows to the proposed onsite full-spectrum detention basin (DB). Specifically,

the 100-year flows from subbasins NW-PR1 through NW-PR5 will be captured and conveyed to the proposed onsite DB.

The surface runoff from Niwot Road (subbasin NW-PR6) will be captured and conveyed in a roadside ditch and combine with the offsite flows from the CDOT median area (south of Niwot Road) conveyed by the existing 18" RCP under Niwot Road. The combined flows will bypass the onsite DB and discharge directly into the existing CDOT water quality basin. Flows from CO 119 NB and SB lanes (subbasins NW-PR7 and NW-PR8) will also bypass the onsite DB and discharge directly into the existing CDOT water quality basin.

All proposed storm drain (SD) inlets and pipes are designed to sufficiently handle the computed 100-year design flows for the proposed site development conditions as summarized in the SD system design flow rates table in Appendix G. In accordance with the RTD P-n-R design criteria, the proposed SD inlets will be designed to capture the 100-year flows with maximum ponding depths of 6 inches or less.

The proposed SD pipes were initially sized based on normal depth calculations using Bentley FlowMaster V8i for the Preliminary Drainage Report. The MHFD's UDSewer program will be used to check the HGL/EGL elevations for the proposed storm drain systems for the Final Drainage Report. Per RTD's design criteria, the minimum SD pipe size used in the proposed P-n-R project will be 18" RCP.

3. Detention and Water Quality Basin

A new onsite full spectrum detention basin (DB) will be provided to capture and route flows from subbasins NW-PR1 through NW-PR5 (up to the 100-year design storm event). The total contributing drainage area for the proposed onsite DB is approximately 2.98 acres with approximately 81.1 percent impervious areas. The MHFD full spectrum detention basin design program, MHFD-Detention, Version 4.05, was used to perform preliminary analysis of the proposed onsite DB. (See detention basin calculations in Appendix F). The outflows from the onsite DB will discharge directly into the existing CDOT water quality basin.

The computed water quality capture volume (WQCV), excess urban runoff volume (EURV), and 100-year detention storage volume will be provided in the proposed full-spectrum onsite detention basin (DB) as summarized in the table below. An emergency overflow spillway will be provided along the improved earthen embankment between the proposed onsite DB and the existing CDOT water quality basin.

Design Event	Total Required Volume (ac. ft.)	
WQCV	0.083	
EURV	0.237	
100-year	0.411	

As summarized in the table below, the proposed conditions 100year combined peak flow rate from the proposed subbasins NW-PR1 through NW-PR8 is less than the existing conditions 100-year peak flow rate of 15.5 cfs from basin NW-EX1.

Basin ID	Q100 (cfs)	
DB Outflow (NW-PR1 through NW-PR5)	3.1	
NW-PR6	3.1	
NW-PR7	3.9	
NW-PR8	2.9	
Total	13.0	

B. 63rd Street P-n-R

1. Proposed Drainage Basins

The proposed conditions drainage subbasin boundaries (63-PR1 through 63-PR8) have been delineated to reflect the proposed site improvement conditions (see Figure 5, Appendix D). In general, the 100-year flows from the proposed RTD P-n-R improvements (63-PR1 through 63-PR5) including bus ramps, station platforms, and P-n-R parking lot will be captured and conveyed to the proposed onsite full spectrum detention basin (DB). However, some portions of CO 119 lanes that surface drain into the proposed bus ramps will also be captured and conveyed to the proposed onsite DB. Surface runoffs from the remaining 63rd Street and CO 119 NB and SB lanes (63-PR6 through 63-PR8) will flow directly into the proposed 10'x6' concrete box culvert (CBC).

The proposed adjacent paved bike trail area (approximately 8144 sf) will drain north to new sump pumps at the low point of the 63rd Street trail underpass. This bike trail area is excluded from RTD's P-n-R proposed conditions hydrologic analysis since the trail area will not drain into RTD's onsite storm drainage and detention systems and the location of the sump pump discharge outfall has

not been identified at the current stage of the trail design.

2. Storm Drain Improvements

The proposed P-n-R onsite storm drain systems are sized to capture and convey the computed 100-year peak flows to the proposed onsite full-spectrum detention basin (DB). Specifically, the 100-year flows from subbasins 63-PR1 through 63-PR5 will be captured and conveyed to the proposed onsite DB. The surface runoff from 63rd Street (subbasin 63-PR7) and CO 119 NB and SB lanes (subbasins 63-PR6 and 63-PR8) will bypass the onsite DB and discharge directly into the proposed 10'x6' CBCs. The offsite flows from basin P172C will also bypass the proposed DB and connect directly to the 10'x6' CBCs.

All proposed storm drain (SD) inlets and pipes are designed to sufficiently handle the computed 100-year design flows for the proposed site development conditions as summarized in the SD system design flow rates table in Appendix G. In accordance with the RTD P-n-R design criteria, the proposed SD inlets will be designed to capture the 100-year flows with maximum ponding depths of 6 inches or less.

The proposed SD pipes were initially sized based on normal depth calculations using Bentley FlowMaster V8i for the Preliminary Drainage Report. The MHFD's UDSewer program will be used to check the HGL/EGL elevations for the proposed storm drain systems for the Final Drainage Report. Per RTD's design criteria, the minimum SD pipe size used in the proposed P-n-R project will be 18" RCP.

3. Detention and Water Quality Basin

A new onsite full spectrum detention basin (DB) will be provided to capture and route flows from subbasins 63-PR1 through 63-PR5 (up to the 100-year design storm event). The total contributing drainage area for the proposed onsite DB is approximately 3.52 acres with approximately 72.8 percent impervious areas. The MHFD full spectrum detention basin design program, MHFD-Detention, Version 4.05, was used to perform preliminary analysis of the proposed onsite DB. (See detention basin calculations in Appendix F). The outflow from the onsite DB will combine with flows from subbasin 63-PR8 and offsite basin P172C and discharge into the proposed 10'x6' CBC.

The computed water quality capture volume (WQCV), excess urban

runoff volume (EURV), and 100-year detention storage volume will be provided in the proposed full-spectrum onsite detention basin (DB) as summarized in the table below. An emergency overflow spillway will be provided along the eastern embankment of the proposed onsite DB.

Design Event	Required Total Volume (ac. ft.)	
WQCV	0.084	
EURV	0.249	
100-year	0.433	

As summarized in the table below, the proposed conditions 100year combined peak flow rate from the proposed subbasins 63-PR1 through 63-PR8 is less than the existing conditions 100-year peak flow rate of 17.3 cfs from basin 63-EX1.

Basin ID	Q100 (cfs)	
DB Outflow	3.1	
(63-PR1 through 63-PR5)		
63-PR6	3.7	
63-PR7	5.8	
63-PR8	2.5	
Total	15.1	

V. CONCLUSIONS

As previously discussed in sections above in detail, the design of drainage facilities for the proposed RTD's P-n-Rs at both 63rd Street and Niwot Road locations will be in general compliance with the Boulder County Storm Drainage Criteria Manual and MHFD's Urban Storm Drainage Criteria Manual (References 2 and 3). The proposed drainage improvements will provide the required flood protection for the RTD's P-n-R facilities.

VI. REFERENCES

- 1. NOAA Atlas 14 Precipitation Frequency Atlas of the United States, Volume 8, Version 2, National Oceanic and Atmospheric Administration (NOAA), 2013.
- 2. Boulder County Storm Drainage Criteria Manual, November 2016.
- 3. Urban Storm Drainage Criteria Manual, Urban Drainage and Flood Control District, Volumes 1 and 2, Updated January 2016 and Volume 3, Updated November 2010.
- 4. CO 119 Safety and Mobility Improvement Project, Preliminary Drainage Report, August 2022, Muller Engineering Company.

APPENDIX

- A. LOCATION MAP
- B. FEMA FIRMETTE
- C. NRCS SOILS MAPS
- D. DRAINAGE BASIN DELINEATION MAPS
- E. HYDROLOGIC CALCULATIONS
- F. DETENTION BASIN DESIGN CALCULATIONS
- G. STORM DRAIN SYSTEM CALCULATIONS
- H. FIR DRAINAGE PLANS

APPENDIX A

LOCATION MAP



APPENDIX B

FEMA FIRMETTE

Attachment D: CO 119 RTD Park-n-Ride Drainage Report National Flood Hazard Layer FIRMette



Legend

105°10'55"W 40°6'21"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X T2N R70W S25 Niwot Road P-n-R Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation AREAOF MINIMAL FLOOD HAZARD Boulder County **Coastal Transect** Base Flood Elevation Line (BFE) 080023 Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** OTHER **Profile Baseline** 08013C0410J FEATURES Hydrographic Feature eff. 12/18/201 **Digital Data Available** No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. This map complies with FEMA's standards for the use of T2N R70W S36 digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/21/2022 at 6:18 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 105°10'18"W 40°5'54"N Feet 1:6,000 unmapped and unmodernized areas cannot be used for regulatory purposes. 250 500 1,000 1,500 2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020





Attachment D: CO 119 RTD Park-n-Ride Drainage Report National Flood Hazard Layer FIRMette



Legend



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



APPENDIX C

NRCS SOILS MAPS



Conservation Service

Hydrologic Soil Group-Boulder County Area, Colorado (Niwot Rd Station)



USDA

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
NnA	Nunn sandy clay loam, 0 to 1 percent slopes	С	57.2	40.7%
NnB	Nunn sandy clay loam, 1 to 3 percent slopes	С	57.9	41.2%
NuB	Nunn clay loam, 1 to 3 percent slopes	С	25.6	18.2%
Totals for Area of Intere	st	140.6	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

Attachment D: CO 119 RTD Park-n-Ride Drainage Report



Conservation Service

Web Soil Survey National Cooperative Soil Survey 3/2/2022 Page 1 of 4

Hydrologic Soil Group—Boulder County Area, Colorado (63rd Street Station)



USDA

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
LoB	Longmont clay, 0 to 3 percent slopes	D	44.3	48.1%
SeE	Samsil-Shingle complex, 5 to 25 percent slopes	D	47.8	51.9%
Totals for Area of Intere	st	92.1	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified Tie-break Rule: Higher

APPENDIX D

DRAINAGE BASIN DELINEATION MAPS









CO119 SAFETY &	Project No./Code		
PROPOSED DRAI			
signer:	Structure		
tailer:	Numbers		
eet Subset:	Subset Sheets:		FIGURE 5

APPENDIX E

HYDROLOGIC CALCULATIONS
															Calcula	tion of P	eak Runo	ff using R	ational N	1ethod															
Designer Company Date Project Location	Yong Sor RTD 7/26/2022 SH 119 E Niwot Ro	ig RT ad Station - RT	D PnR	Cells o Cells o Cells o	of this color of this color of this color of this color	are for requ are for optic are for calc	017 nired user-inp onal override ulated result	values s based on	overrides	t _i =	$\frac{0.395(1.1 - C_s)}{S_t^{0.33}} = \frac{L_t}{60K\sqrt{S_t}} = \frac{1}{60}$	v v	Computed	$t_c = t_i + t_t$ $t_c = (26 - 17i)$	$+\frac{L_t}{60(14i+9)}$	$\sqrt{S_t}$	$t_{minimum} = 5$ $t_{minimum} = 1$ Selected $t_c =$	(urban) O (non-urban) = max{t _{minimur}	n , min (Compu	ted t _c , Regiona	ul t _e)}	1 Rainfall Inter	Select	UDFCD location depth, P1 (in) = Coefficients =	2-yr 0.79 8 28.50	Atlas 14 Rainfa 5-yr 10 1.07 1 b 10.00 0.	Depths fro -yr 25- 35 1.8 c I(in 786	$\frac{\text{m the pulldor}}{\text{yr}} = \frac{3}{(b + r)}$	100-yr 2.69 P ₁ t _c) ^c	500-yr 3.98	n depths obtaine	d from the	Q(cfs) = 1	e (dick this	: link)
	1				Ru	noff Coeffi	cient, C				Overla	nd (Initial) Flo	w Time		1		Channel	ized (Travel) Fl	low Time			Tim	e of Concentr	ation		Ra	infall Inten	sity, I (in/hr)				1	Peak Flow, Q	(cfs)	
Subcatchment Name	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousnes s	2-yr 5-y	10-y	25-yr	50-yr	100-yr	500-yr	Overland Flow Length L _i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope S _i (ft/ft)	Overland Flow Time t _i (min)	Channelized Flow Length L _t (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)	Channelized Flow Time t _t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	2-yr	5-yr 10	-yr 25-	yr 50-yr	100-yr	500-yr	2-yr 5-y	r 10-)	yr 25-yr	50-yr	100-yr 500-yr
NW-EX1	4.54	с	46.1	0.35 0.4	1 0.47	0.58	0.62	0.67	0.73	125.00	5112.14	5109.00	0.025	10.27	500.00	5109.00	5103.50	0.011	7	0.73	11.35	21.62	23.30	21.62	1.49	2.02 2	55 3.4	2 4.21	5.08	7.51	2.37 3.7	7 5.4	5 8.96	11.87	15.51 25.02
						_																						_					_		
				0.81 0.8	3 0.85	0.86	0.87	0.88	0.89		-			6.62								7.75		7.75	2.35	3.18 4	01 5.3	8 6.63	7.99	11.83	0.90 1.2	5 16	1 221	2.75	3.35 5.02
NW-PR1	0.48	С	97.2	0.01 0.0	0.00	0.00	0.07	0.00	0.00	178.00	5109.99	5108.25	0.010	0.02	97.00	5108.25	5107.75	0.005	20	1.44	1.13	1.10	10.47	1.10	2.00	0.10 4	01 0.0	0.00	1.00	11.00	0.00 1.1	0 1.0		2.10	0.00 0.01
NW-PR2	0.55	с	86.2	0.71 0.7	1 0.77	0.80	0.82	0.84	0.86	127.00	5109.99	5108.16	0.014	6.54	69.00	5108.16	5107.80	0.005	20	1.44	0.80	7.33	12.10	7.33	2.39	3.24 4	09 5.4	8 6.75	8.14	12.05	0.92 1.3	0 1.7	1 2.40	3.02	3.72 5.65
NW-PR3	0.99	с	92.2	0.76 0.7	9 0.81	0.84	0.85	0.86	0.88	135.00	5112.13	5109.29	0.021	5.15	438.00	5109.29	5106.25	0.007	20	1.67	4.38	9.53	14.33	9.53	2.18	2.95 3	72 4.9	9 6.15	7.42	10.97	1.64 2.2	9 2.9	8 4.12	5.15	6.31 9.52
NW-PR4	0.46	С	100.0	0.83 0.8	5 0.87	0.88	0.89	0.89	0.90	138.00	5111.40	5109.20	0.016	4.55	238.00	5109.20	5107.55	0.007	20	1.67	2.38	6.93	11.07	6.93	2.44	3.30 4	16 5.5	i8 6.88	8.30	12.28	0.94 1.3	0 1.6	7 2.27	2.82	3.43 5.13
		-		0.14 0.2	0.29	0.44	0.50	0.57	0.65		-																	-		-			-		
NW-PR5 (DB)	0.50	C	20.9																															4	
NW-PR6	0.47	С	79.1	0.64 0.6	3 0.71	0.76	0.78	0.81	0.84	129.00	5111.40	5109.29	0.016	7.33	20.00	5109.29	5106.60	0.134	15	5.50	0.06	7.39	12.60	7.39	2.39	3.23 4	08 5.4	6.73	8.12	12.02	0.71 1.0	2 1.3	5 1.94	2.45	3.05 4.68
NW-PR7	0.54	с	95.9	0.80 0.8	2 0.84	0.86	0.87	0.88	0.89	90.00	5112.10	5109.60	0.028	3.47	335.00	5109.60	5107.47	0.006	20	1.59	3.50	6.97	12.82	6.97	2.44	3.29 4	16 5.5	6.87	8.28	12.25	1.05 1.4	6 1.8	9 2.59	3.23	3.93 5.91
NW-PR8	0.37	С	100.0	0.83 0.8	5 0.87	0.88	0.89	0.89	0.90	92.00	5110.82	5109.35	0.016	3.71	212.00	5109.35	5108.12	0.006	20	1.52	2.32	6.03	11.02	6.03	2.55	3.44 4	35 5.8	13 7.18	8.66	12.81	0.78 1.0	8 1.3	9 1.89	2.35	2.85 4.27

NIWOT ROAD P-n-R

EXISTING CONDITIONS DRAINAGE BASINS

Basin ID	Total Area (sq. ft.)	Total Area (acres)	Landscaped Area (sq. ft.)	Paved Area (sq. ft.)	% Landscaped Area	% Paved Area	Note
NW-EX1	197,881	4.543	106,687	91,194	53.9	46.1	

PROPOSED CONDITIONS DRAINAGE BASINS

Basin ID	Total Area (sq. ft.)	Total Area (acres)	Landscaped Area (sq. ft.)	Paved Area (sq. ft.)	% Landscaped Area	% Paved Area	Note
NW - PR1	20,680	0.475	577	20,103	2.8	97.2	
NW - PR2	23,799	0.546	3,282	20,517	13.8	86.2	
NW - PR3	43,043	0.988	3,354	39,689	7.8	92.2	
NW - PR4	20,175	0.463	0	20,175	0.0	100.0	
NW - PR5	21,911	0.503	17,336	4,575	79.1	20.9	
Total DB Contributing Basins	129,608	2.975	24,549	105,059	18.9	81.1	Excludes paved bike trail area (5960 sf) - which drains south to sump pumps near Niwot Road underpass
NW - PR6	20,256	0.465	4,230	16,026	20.9	79.1	
NW - PR7	23,605	0.542	972	22,633	4.1	95.9	
NW - PR8	16,086	0.369	0	16,086	0.0	100.0	
Total Niwot Basins	189,555	4.352	29,751	159,804	15.7	84.3	

Back up Calc for UD Detention

Proposed P-n-R Site

H (ft)	L (ft)	Slope (ft/ft)	LC (ft)
5.88	573	0.010	156

Attachment D: CO 119 RTP Park-n-Ride Drh Age Ratios 14, Volume 8, Version 2



Latitude: 40.1019°, Longitude: -105.1769° Elevation: 5108.03 ft** source: ESRI Maps ** source: USGS

Location name: Longmont, Colorado, USA*



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹ Average recurrence interval (years)														
Duration				Average	recurrence	interval (ye	ears)								
Duration	1	2	5	10	25	50	100	200	500	1000					
5-min	0.218	0.265	0.359	0.453	0.608	0.748	0.904	1.08	1.34	1.56					
	(0.176-0.272)	(0.213-0.331)	(0.288-0.450)	(0.361-0.571)	(0.477-0.825)	(0.565-1.02)	(0.655-1.26)	(0.744-1.54)	(0.881-1.96)	(0.985-2.27)					
10-min	0.319	0.387	0.525	0.664	0.891	1.10	1.32	1.58	1.96	2.28					
	(0.257-0.399)	(0.312-0.485)	(0.421-0.659)	(0.529-0.836)	(0.699-1.21)	(0.827-1.49)	(0.959-1.84)	(1.09-2.26)	(1.29-2.87)	(1.44-3.33)					
15-min	0.389	0.472	0.640	0.809	1.09	1.34	1.61	1.93	2.39	2.78					
	(0.314-0.486)	(0.380-0.591)	(0.514-0.803)	(0.645-1.02)	(0.852-1.47)	(1.01-1.82)	(1.17-2.25)	(1.33-2.75)	(1.57-3.50)	(1.76-4.06)					
30-min	0.529	0.641	0.867	1.10	1.47	1.81	2.18	2.61	3.24	3.76					
	(0.427-0.661)	(0.516-0.802)	(0.695-1.09)	(0.872-1.38)	(1.15-1.99)	(1.37-2.46)	(1.58-3.04)	(1.80-3.73)	(2.13-4.74)	(2.38-5.50)					
60-min	0.652	0.791	1.07	1.35	1.81	2.23	2.69	3.21	3.98	4.61					
	(0.525-0.814)	(0.637-0.990)	(0.859-1.34)	(1.08-1.71)	(1.42-2.46)	(1.68-3.03)	(1.95-3.74)	(2.21-4.58)	(2.62-5.81)	(2.92-6.74)					
2-hr	0.774	0.941	1.28	1.61	2.16	2.65	3.19	3.81	4.71	5.46					
	(0.629-0.958)	(0.764-1.17)	(1.03-1.59)	(1.29-2.01)	(1.71-2.89)	(2.02-3.56)	(2.33-4.40)	(2.65-5.38)	(3.13-6.82)	(3.50-7.91)					
3-hr	0.847	1.03	1.40	1.76	2.34	2.86	3.44	4.10	5.05	5.85					
	(0.692-1.04)	(0.841-1.27)	(1.13-1.72)	(1.42-2.18)	(1.86-3.12)	(2.19-3.83)	(2.53-4.71)	(2.87-5.75)	(3.38-7.27)	(3.77-8.42)					
6-hr	1.02	1.23	1.65	2.05	2.70	3.28	3.91	4.62	5.66	6.52					
	(0.840-1.24)	(1.01-1.50)	(1.35-2.02)	(1.67-2.52)	(2.16-3.55)	(2.53-4.33)	(2.90-5.29)	(3.27-6.41)	(3.83-8.05)	(4.25-9.29)					
12-hr	1.27	1.52	2.00	2.45	3.17	3.80	4.48	5.25	6.35	7.26					
	(1.05-1.53)	(1.26-1.83)	(1.65-2.41)	(2.01-2.98)	(2.55-4.10)	(2.95-4.94)	(3.35-5.98)	(3.74-7.18)	(4.33-8.92)	(4.78-10.2)					
24-hr	1.51	1.84	2.43	2.97	3.79	4.47	5.20	5.99	7.11	8.01					
	(1.26-1.80)	(1.54-2.20)	(2.03-2.92)	(2.46-3.58)	(3.05-4.80)	(3.49-5.72)	(3.91-6.82)	(4.30-8.07)	(4.89-9.85)	(5.34-11.2)					
2-day	1.70	2.14	2.89	3.53	4.45	5.18	5.94	6.74	7.83	8.68					
	(1.44-2.01)	(1.81-2.54)	(2.42-3.43)	(2.95-4.21)	(3.59-5.52)	(4.07-6.52)	(4.50-7.66)	(4.87-8.93)	(5.43-10.7)	(5.85-12.0)					
3-day	1.86 (1.58-2.18)	2.31 (1.95-2.71)	3.07 (2.59-3.61)	3.72 (3.12-4.40)	4.66 (3.77-5.74)	5.41 (4.27-6.75)	6.18 (4.70-7.92)	6.99 (5.09-9.21)	8.10 (5.66-11.0)	8.97 (6.09-12.3)					
4-day	2.00	2.43	3.18	3.82	4.76	5.51	6.29	7.11	8.25	9.14					
	(1.70-2.33)	(2.07-2.85)	(2.69-3.73)	(3.22-4.51)	(3.87-5.84)	(4.37-6.86)	(4.81-8.03)	(5.21-9.34)	(5.79-11.1)	(6.23-12.5)					
7-day	2.34 (2.00-2.71)	2.75 (2.35-3.19)	3.47 (2.96-4.04)	4.10 (3.47-4.79)	5.02 (4.13-6.12)	5.77 (4.62-7.13)	6.56 (5.06-8.31)	7.39 (5.46-9.63)	8.55 (6.06-11.5)	9.47 (6.52-12.8)					
10-day	2.62	3.04	3.76	4.39	5.31	6.06	6.84	7.67	8.82	9.74					
	(2.25-3.02)	(2.61-3.51)	(3.22-4.35)	(3.73-5.10)	(4.38-6.43)	(4.87-7.43)	(5.31-8.61)	(5.70-9.93)	(6.29-11.8)	(6.74-13.1)					
20-day	3.38	3.86	4.67	5.36	6.33	7.10	7.89	8.71	9.82	10.7					
	(2.93-3.86)	(3.35-4.41)	(4.03-5.35)	(4.60-6.16)	(5.26-7.54)	(5.76-8.58)	(6.18-9.79)	(6.53-11.1)	(7.07-12.9)	(7.48-14.3)					
30-day	3.99	4.56	5.49	6.27	7.33	8.15	8.98	9.81	10.9	11.8					
	(3.48-4.52)	(3.97-5.17)	(4.77-6.25)	(5.41-7.16)	(6.11-8.64)	(6.64-9.76)	(7.06-11.0)	(7.39-12.4)	(7.91-14.2)	(8.29-15.6)					
45-day	4.74 (4.15-5.33)	5.44 (4.77-6.13)	6.58 (5.74-7.43)	7.49 (6.50-8.51)	8.72 (7.29-10.2)	9.65 (7.88-11.4)	10.5 (8.33-12.8)	11.4 (8.66-14.3)	12.6 (9.16-16.3)	13.4 (9.54-17.7)					
60-day	5.37	6.20	7.53	8.59	9.98	11.0	12.0	13.0	14.2	15.1					
	(4.72-6.02)	(5.45-6.96)	(6.59-8.47)	(7.48-9.70)	(8.36-11.6)	(9.03-13.0)	(9.51-14.5)	(9.86-16.2)	(10.4-18.2)	(10.8-19.8)					

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

Attachment D: CO 119 RTD Park-n-Ride Drainage Report





NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Mon Jun 6 21:38:25 2022

interval (years)

> - 1 2

> > 5 10

> > > 25 50

100 200

500

- 1000

2-day

3-day

4-day 7-day

10-day

20-day

30-day

- 45-day

60-day

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Maps & aerials

Small scale terrain



Large scale terrain





Large scale aerial



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																Calcula	tion of P	eak Runo	ff using R	ational N	1ethod																
Designe Company Date Projec Location	Yong Son RTD 7/27/2022 SH 119 B 63rd Stree	g RT et Station - RTI	D PnR	Vers Cell Cell	on 2.00 re s of this co s of this co s of this co	blor are for blor are for blor are for	r required of requ	user-inpu override v d results	it values based on	overrides	t _i =	$\frac{0.395(1.1 - C_5}{S_1^{0.33}}$ $= \frac{L_t}{60K\sqrt{S_t}} = \frac{1}{60}$	$\frac{1}{\sqrt{L_i}}$	Compute	$t_c = t_i + t_t$ $t_c = (26 - 17i)$	$+\frac{L_t}{60(14i+9)}$	$\sqrt{S_t}$	$t_{minimum} = 5$ $t_{minimum} = 1$ Selected $t_c = 1$	5 (urban) 10 (non-urban) = max{t _{minimur}	n , min (Compu	ted t _c , Regiona	il t _e)}	f Rainfall Inte	Select	UDFCD location depth, P1 (in) = Coefficients =	for NOAA . 2-yr 0.79 a 28.50	Atlas 14 Rainfa 5-yr 1 1.06 1 b 10.00 0.	I Depths from I-yr 25-y 33 1.7i c I 786 I (in)	$\frac{r}{r} \frac{50 \cdot yr}{2.17}$ $\frac{3}{r} \frac{1}{r}$	100-yr 2.61 2.61 (P ₁ (t _c) ^c	500-yr 3.82	n depths obtain	ined from I	Q(cfs)) = CIA	<u>nis link</u>)	
	1					Runoff C	oefficient	t, C				Overla	nd (Initial) Flo	ow Time				Channel	ized (Travel) F	low Time			Tin	e of Concentr	ation		R	infall Intens	sity, I (in/hr)					Peak Flow	w, Q (cfs)		_
Subcatchmen Name	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousnes s	2-yr 5	-yr 1	0-yr 2	25-yr	50-yr	100-yr	500-yr	Overland Flow Lengt L _i (ft)	u/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	N Overland Flow Slope S ₁ (ft/ft)	Overland Flow Time t _i (min)	Channelized Flow Length L _t (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope S _t (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity V _t (ft/sec)	Channelized Flow Time t _t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	2-yr	5-yr 1	i-yr 25-y	r 50-yr	100-yr	500-yr	2-yr 5	i-yr 1	0-yr 25-	-yr 50-y	r 100-yr 500)0-yr
63-EX1	5.39	D	36.5	0.27 0	.33 C).40 (0.52	0.57	0.63	0.70	252.00	5165.20	5154.00	0.044	13.45	413.00	5154.00	5146.00	0.019	7	0.97	7.07	20.51	23.30	20.51	1.52	2.06 2	58 3.4	6 4.21	5.07	7.42	2.21 3	.68	j.56 9.7	/4 13.0) 17.28 28.	8.07
																-																		_			
63-PR1	0.60	D	88.5	0.73 0	.76 0).78 (0.81	0.83	0.85	0.87	86.00	5156.29	5155.83	0.005	7.08	266.00	5155.83	5154.14	0.006	20	1.59	2.78	9.86	13.56	9.86	2.14	2.88 3	62 4.8	4 5.90	7.10	10.39	0.93 1	.30	1.69 2.5	35 2.97	3.58 5.2	j.37
63-PR2	0.54	D	95.9	0.80 0	.82 0).84 (0.86	0.87	0.88	0.89	69.00	5156.81	5155.47	0.019	3.41	370.00	5155.47	5153.51	0.005	20	1.46	4.24	7.65	13.48	7.65	2.34	3.16 3	97 5.3	1 6.48	7.79	11.40	1.01 1	.40	1.80 2.4	16 3.04	3.69 5.4	5.49
63-PR3	0.64	D	91.0	0.75 0	.78 0	0.80 0	0.83	0.84	0.86	0.87	93.00	5155.48	5154.04	0.015	4.87	220.00	5154.04	5152.96	0.005	20	1.40	2.62	7.49	12.94	7.49	2.36	3.19 4	00 5.3	5 6.52	7.85	11.48	1.12 1	.57 :	2.03 2.8	\$2 3.45	4.27 6.3	j.38
63-PR4	1.21	D	76.7	0.62 0	.66 C).70 (0.75	0.77	0.80	0.83	73.00	5162.13	5158.50	0.050	4.00	523.00	5158.50	5153.15	0.010	20	2.02	4.31	8.31	17.33	8.31	2.28	3.07 3	86 5.1	6 6.29	7.57	11.08	1.70 2	.45	3.24 4.6	37 5.87	7.30 11.	1.11
63-PR5 (DB)	0.53	D	1.3	0.01 0	.05 0).14 (0.33	0.40	0.49	0.59																			_					_			
63-PR6	0.46	D	100.0	0.83 0	.85 0).87 (0.88	0.89	0.89	0.90	74.00	5165.07	5161.25	0.052	2.26	283.00	5161.25	5157.53	0.013	20	2.29	2.06	4.32	10.79	5.00	2.66	3.60 4	51 6.0	4 7.36	8.85	12.96	1.03 1	.41	1.81 2.4	16 3.02	3.66 5.4	i.42
63-PR7	0.93	D	89.3	0.73 0	.76 0).79 (0.82	0.83	0.85	0.87	262.00	5165.30	5155.91	0.036	6.47	267.00	5155.91	5153.67	0.008	20	1.83	2.43	8.90	13.08	8.90	2.22	3.00 3	76 5.0	4 6.14	7.38	10.81	1.52 2	.13 1	2.76 3.8	34 4.76	5.83 8.7	1.74
63-PR8	0.32	D	100.0	0.83 0	.85 0	0.87 0	0.88	0.89	0.89	0.90	45.00	5155.01	5154.45	0.012	2.82	180.00	5154.45	5153.69	0.004	20	1.30	2.31	5.13	11.01	5.13	2.65	3.57 4	48 6.0	0 7.31	8.79	12.87	0.70 0	.97	1.24 1.6	38 2.07	2.51 3.7	1.71

63rd Street RTD P-n-R

EXISTING CONDITIONS DRAINAGE BASINS

Basin ID	Total Area (sq. ft.)	Total Area (acres)	Landscaped Area (sq. ft.)	Paved Area (sq. ft.)	% Landscaped Area	% Paved Area	Note
63-EX1	234,550	5.385	148,983	85,567	63.5	36.5	

PROPOSED CONDITIONS DRAINAGE BASINS

Basin ID	Total Area (sq. ft.)	Total Area (acres)	Landscaped Area (sq. ft.)	Paved Area (sq. ft.)	% Landscaped Area	% Paved Area	Note
63-PR1	25,970	0.596	2,986	22,984	11.5	88.5	
63-PR2	23,551	0.541	964	22,587	4.1	95.9	
63-PR3	27,663	0.635	2,484	25,179	9.0	91.0	
63-PR4	52,683	1.209	12,274	40,409	23.3	76.7	
63-PR5 (DB)	23,273	0.534	22,973	300	98.7	1.3	DB Basin
Total for Basins draining into DB	153,140	3.516	41,681	111,459	27.2	72.8	
		0.000					
63-PR6	20,156	0.463	0	20,156	0.0	100.0	
63-PR7	40,514	0.930	4,327	36,187	10.7	89.3	
63-PR8	13,884	0.319	0	13,884	0.0	100.0	
Total	227,694	5.227	46,008	181,686	20.2	79.8	Exclude bike trail area (8144 sf) which drains into sump pumps at 63rd Street underpass

Back up Calc for UD Detention

Proposed P-n-R Site

H (ft)	L (ft)	Slope (ft/ft)	LC (ft)
8.98	596	0.015	279

Attachment D: CO 119 RTD Park-n-Ride Dra Artige 14, Volume 8, Version 2



Latitude: 40.0742°, Longitude: -105.2073° Elevation: 5151.67 ft** * source: ESRI Maps ** source: USGS

Location name: Boulder, Colorado, USA*



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS	-based po	int precip	itation fre	quency e	stimates v	vith 90% c	onfidenc	e interva	ls (in inc	hes) ¹
Duration				Average	recurrence	interval (yea	ars)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.213	0.260	0.354	0.446	0.595	0.728	0.876	1.04	1.29	1.49
	(0.174-0.264)	(0.212-0.322)	(0.287-0.439)	(0.359-0.556)	(0.470-0.795)	(0.553-0.975)	(0.637-1.20)	(0.720-1.46)	(0.847-1.85)	(0.943-2.14)
10-min	0.312	0.381	0.518	0.653	0.872	1.07	1.28	1.53	1.88	2.18
	(0.255-0.386)	(0.310-0.472)	(0.420-0.642)	(0.526-0.814)	(0.688-1.16)	(0.810-1.43)	(0.933-1.76)	(1.06-2.14)	(1.24-2.70)	(1.38-3.13)
15-min	0.381	0.465	0.631	0.796	1.06	1.30	1.57	1.86	2.30	2.66
	(0.310-0.471)	(0.379-0.576)	(0.512-0.783)	(0.641-0.992)	(0.839-1.42)	(0.988-1.74)	(1.14-2.14)	(1.29-2.61)	(1.51-3.30)	(1.68-3.82)
30-min	0.521	0.635	0.859	1.08	1.45	1.77	2.13	2.53	3.13	3.62
	(0.425-0.644)	(0.516-0.785)	(0.696-1.07)	(0.871-1.35)	(1.14-1.93)	(1.34-2.37)	(1.55-2.91)	(1.75-3.55)	(2.06-4.49)	(2.29-5.20)
60-min	0.645	0.785	1.06	1.33	1.78	2.17	2.61	3.10	3.82	4.41
	(0.525-0.797)	(0.639-0.971)	(0.860-1.32)	(1.07-1.66)	(1.40-2.37)	(1.65-2.90)	(1.90-3.57)	(2.14-4.34)	(2.51-5.48)	(2.79-6.34)
2-hr	0.768	0.935	1.26	1.59	2.11	2.57	3.09	3.66	4.51	5.21
	(0.631-0.941)	(0.767-1.15)	(1.03-1.55)	(1.29-1.96)	(1.68-2.78)	(1.97-3.41)	(2.26-4.18)	(2.55-5.08)	(3.00-6.41)	(3.33-7.41)
3-hr	0.844	1.03	1.38	1.73	2.28	2.77	3.32	3.93	4.82	5.56
	(0.696-1.03)	(0.844-1.25)	(1.13-1.69)	(1.41-2.12)	(1.82-2.99)	(2.13-3.65)	(2.45-4.47)	(2.76-5.42)	(3.23-6.81)	(3.58-7.87)
6-hr	1.02	1.23	1.64	2.03	2.65	3.19	3.79	4.46	5.43	6.24
	(0.851-1.24)	(1.02-1.49)	(1.35-1.98)	(1.66-2.46)	(2.13-3.43)	(2.48-4.16)	(2.82-5.05)	(3.16-6.09)	(3.68-7.61)	(4.07-8.75)
12-hr	1.28	1.53	2.00	2.45	3.15	3.76	4.43	5.17	6.23	7.11
	(1.07-1.53)	(1.28-1.83)	(1.67-2.40)	(2.03-2.95)	(2.55-4.03)	(2.94-4.84)	(3.32-5.83)	(3.69-6.98)	(4.26-8.63)	(4.69-9.89)
24-hr	1.53	1.86	2.47	3.01	3.83	4.52	5.25	6.04	7.15	8.05
	(1.29-1.81)	(1.57-2.21)	(2.07-2.93)	(2.51-3.60)	(3.10-4.81)	(3.55-5.72)	(3.96-6.81)	(4.35-8.04)	(4.93-9.78)	(5.37-11.1)
2-day	1.72	2.17	2.95	3.61	4.56	5.31	6.09	6.90	8.01	8.87
	(1.46-2.01)	(1.85-2.55)	(2.49-3.47)	(3.04-4.27)	(3.69-5.61)	(4.19-6.62)	(4.63-7.77)	(5.01-9.05)	(5.56-10.8)	(5.99-12.1)
3-day	1.87	2.34	3.13	3.81	4.77	5.54	6.34	7.17	8.31	9.20
	(1.60-2.18)	(1.99-2.73)	(2.66-3.66)	(3.21-4.47)	(3.89-5.83)	(4.40-6.86)	(4.85-8.05)	(5.24-9.35)	(5.81-11.1)	(6.25-12.5)
4-day	2.02	2.47	3.24	3.90	4.86	5.64	6.45	7.29	8.46	9.38
	(1.73-2.34)	(2.11-2.87)	(2.76-3.77)	(3.30-4.57)	(3.98-5.93)	(4.50-6.96)	(4.95-8.15)	(5.35-9.48)	(5.95-11.3)	(6.41-12.7)
7-day	2.38	2.80	3.52	4.16	5.10	5.87	6.69	7.55	8.76	9.72
	(2.05-2.74)	(2.41-3.23)	(3.02-4.07)	(3.55-4.83)	(4.22-6.18)	(4.73-7.21)	(5.18-8.41)	(5.60-9.76)	(6.23-11.6)	(6.70-13.1)
10-day	2.68	3.10	3.81	4.45	5.38	6.15	6.96	7.82	9.02	9.98
	(2.32-3.08)	(2.68-3.55)	(3.28-4.39)	(3.81-5.14)	(4.47-6.48)	(4.97-7.50)	(5.42-8.70)	(5.83-10.0)	(6.45-11.9)	(6.92-13.3)
20-day	3.47	3.95	4.76	5.45	6.43	7.21	8.01	8.85	9.99	10.9
	(3.03-3.94)	(3.44-4.49)	(4.13-5.42)	(4.70-6.23)	(5.37-7.62)	(5.87-8.66)	(6.30-9.87)	(6.66-11.2)	(7.21-13.0)	(7.64-14.4)
30-day	4.09	4.67	5.61	6.40	7.47	8.30	9.14	9.98	11.1	11.9
	(3.59-4.62)	(4.09-5.27)	(4.89-6.35)	(5.54-7.27)	(6.25-8.76)	(6.79-9.88)	(7.21-11.2)	(7.54-12.5)	(8.06-14.3)	(8.45-15.7)
45-day	4.87 (4.29-5.46)	5.59 (4.92-6.28)	6.74 (5.91-7.59)	7.68 (6.69-8.68)	8.93 (7.49-10.4)	9.86 (8.09-11.6)	10.8 (8.54-13.0)	11.7 (8.86-14.5)	12.8 (9.36-16.4)	13.7 (9.74-17.9)
60-day	5.53 (4.89-6.18)	6.39 (5.64-7.14)	7.74 (6.80-8.67)	8.82 (7.71-9.93)	10.2 (8.61-11.8)	11.3 (9.29-13.2)	12.3 (9.78-14.8)	13.3 (10.1-16.5)	14.5 (10.6-18.5)	15.4 (11.0-20.1)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

Attachment D: CO 119 RTD Park-n-Ride Drainage Report





	1000
Dura	ation
— 5-min	— 2-day
— 10-min	— 3-day
- 15-min	— 4-day

30-min

60-min

2-hr

3-hr

6-hr

12-hr

24-hr

7-day

10-day

20-day

30-day

45-day

60-day

Average recurrence

interval (years)

- 1

5 10

25

50 100 200

500

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Maps & aerials

Small scale terrain





Large scale terrain



40 Fort Collins Greeley Longmont Benver to Colorado Springs

Large scale aerial



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

APPENDIX F

DETENTION BASIN DESIGN CALCULATIONS

Attachment D: CO 119 RTD Park-n-Ride Drainage Report

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)
Project: SH119 BRT - Niwot Road Station PnR

Basin ID:	Proposed (Condition B	asins PR1 th	ru PR5										
ZONE 3	2													
100-711	TONIE 1	T												
VOLUME SURV MOCY	1	-		~										
	1	100-11	EAR .		Depth Increment =		ft							
PERMANENT ORIFI	CES	Lines					Optional				Optional			
Poor Example Zon	e Configura	ation (Rete	ntion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area (acro)	Volume	Volume
Watershed Information					Top of Micropool		0.00					0.000	(11)	(ac-it)
Colorted DMD Ture	EDR				Top of Theropool		0.00				5 374	0.101	1 210	0.020
Selected BMP Type =	EDB	_					0.50	-		-	5,2/4	0.121	1,318	0.030
Watershed Area =	2.98	acres					1.00	-		-	8,182	0.188	4,682	0.107
Watershed Length =	573	ft					1.50	-			9,034	0.207	8,986	0.206
Watershed Length to Centroid =	156	ft					2.00	-			9,992	0.229	13,743	0.315
Watershed Slope =	0.010	ft/ft					2.50	-		-	10,930	0.251	18,973	0.436
Watershed Imperviousness =	81.10%	percent					3.00				11,957	0.274	24,695	0.567
Percentage Hydrologic Soil Group A =	0.0%	percent					3.50				13,000	0.298	30,934	0.710
Percentage Hydrologic Soil Group B =	0.0%	percent					4.00				14,063	0.323	37,700	0.865
Percentage Hydrologic Soil Groups C/D =	100.0%	percent					4.50				15.000	0.344	44,966	1.032
Target WOCV Drain Time =	40.0	hours											1	
Location for 1-hr Rainfall Depths =	User Input													
A day and day and include the start in	ali alian di kana													
depths, click 'Run CUHP' to generate run	off hydrogram	hs using												
the embedded Colorado Urban Hydro	ograph Proced	lure.	Ontional Use	ar Overridec						-				
Water Quality Canture Volume (WOCV) -	0.083	acre-feet	Optional 030	acre-feet		-		_						
Excess Lithan Runoff Volume (FURV) =	0.005	acro foot		acro foot										
2 Duraff Values (D1 - 0.70 in)	0.237	acre-leet	0.70	acre-reet				-		-				
2-yr Kuloir Volume (P1 = 0.75 III.) =	0.141	acrefieer	0.79	inches				-		-				
$_{3-y_1}$ reaction volume (P1 = 1.0/ In.) =	0.202	aure-reet	1.07	linches			-	-			-		1	
10-yr Kurioli Volume (P1 = 1.35 in.) =	0.269	acre-reet	1.35	incries				-						
25-yr kunorr Volume (P1 = 1.81 in.) =	0.386	acre-teet	1.81	incnes						-			<u> </u>	
50-yr Runoff Volume (P1 = 2.23 in.) =	0.491	acre-feet	2.23	inches						-			l	
100-yr Runoff Volume (P1 = 2.69 in.) =	0.609	acre-feet	2.69	inches						-				
500-yr Runoff Volume (P1 = 3.98 in.) =	0.935	acre-feet	3.98	inches				-		-				
Approximate 2-yr Detention Volume =	0.143	acre-feet						-		-				
Approximate 5-yr Detention Volume =	0.208	acre-feet								-				
Approximate 10-yr Detention Volume =	0.260	acre-feet												
Approximate 25-yr Detention Volume =	0.323	acre-feet												
Approximate 50-yr Detention Volume =	0.362	acre-feet								-				
Approximate 100-yr Detention Volume =	0.411	acre-feet						-		-				
								-						
Define Zones and Basin Geometry														
Zone 1 Volume (WOCV) =	0.083	acre-feet						-						
Zone 2 Volume (EURV - Zone 1) =	0.154	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	0 174	acre-feet												
Total Detention Basin Volume =	0.411	acre-feet												
Initial Surcharge Volume (ISV) -	USOr	4 3								-				
Initial Scientinge Volume (ISV) =	user	a.												
Initial Surcharge Depth (ISD) =	user	п. 						-		-				
Total Available Detention Depth (H _{total}) =	user							-		-				
Depth of Inckle Channel $(H_{TC}) =$	user	ft								-				
Slope of Trickle Channel (STC) =	user	ft/ft								-				
Slopes of Main Basin Sides (S _{main}) =	user	H:V												
Basin Length-to-Width Ratio (R _{L/W}) =	user													
		_						-						
Initial Surcharge Area (A _{ISV}) =	user	ft ²						-						
Surcharge Volume Length $(L_{ISV}) =$	user	ft						-						
Surcharge Volume Width $(W_{ISV}) =$	user	ft						-						
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft						-						
Length of Basin Floor $(L_{FLOOR}) =$	user	ft						-		-				
Width of Basin Floor (W _{FLOOR}) =	user	ft						-						
Area of Basin Floor (A _{FLOOR}) =	user	ft ²												
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³												
Depth of Main Basin (H _{MATN}) =	user	ft												
Length of Main Basin (LMATN) =	user	ft												
Width of Main Basin (WMAIN) =	user	ft												
Area of Main Basin (Aman) =	user	ft ²												
Volume of Main Basin (VMATA) =	user	ft ³												
Calculated Total Basin Volume (V) =	user	acre-feet								-				
(total)										-				
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MHFD-Detention, Version 4.05 (January 2022)



	DF	TENTION	RASIN OUT	I FT STRU		SIGN									
			FD-Detention, Ver	sion 4.05 (Januar	<i>2022)</i>										
Project:	SH119 BRT - Niwe	t Road Station PnF	2												
Basin 1D: ZONE 3	Proposed Condition	on Basins PR1 thru	PR5												
		~		Estimated Stage (ft)	Estimated Volume (ac-ft)	Outlet Type									
			Zone 1 (WQCV)	0.87	0.083	Orifice Plate									
	100-YEAR ORIFICE		Zone 2 (EURV)	1.65	0.154	Orifice Plate									
PERMANENT ORIFICES	C -firmation (De	(diam Dand)	Zone 3 (100-year)	2.41	0.174	Weir&Pipe (Restrict)									
	Contiguration (re	tention Policy		Total (all zones)	0.411		C. Inc. Include Development	· · · · · · · · · · · · · · · · · · ·							
User Input: Orifice at Underdrain Outlet (typican)	N/A	ft (distance below	<u>1P)</u> the filtration media	surface)	Underg	Irain Orifice Area =	N/A	eters for Underdram							
Underdrain Orifice Diameter =	N/A	inches	the models mean	Surrace	Underdrair	Orifice Centroid =	N/A	feet							
User Input: Orifice Plate with one or more orifice	es or Elliptical Slot	Neir (typically used	to drain WQCV and	I/or EURV in a sedi	mentation BMP)		Calculated Parame	ters for Plate							
Centrold of Lowest Unlice =	0.00	ft (relative to basin ft (relative to basin	bottom at Stage =	0 ft) 0 ft)	WQ Orm Fili	ce Area per Kow =	6.944E-03 N/A	ft ² foot							
Orifice Plate: Orifice Vertical Spacing =	8.00	inches	bottom at bitage	0.0	Ellipt	ical Slot Centroid =	N/A	feet							
Orifice Plate: Orifice Area per Row =	1.00	sq. inches (diamete	er = 1-1/8 inches)		E	lliptical Slot Area =	N/A	ft²							
User Input: Stage and Total Area of Each Orifice	Row (numbered f	om lowost to higho	ct)												
User Input. Stage and Total Area of Each Office	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	l						
Stage of Orifice Centroid (ft)	0.00	0.70	1.40			(())	(()))))))))))))))))))))))))))))))))))))								
Orifice Area (sq. inches)	1.00	1.00	1.00												
									l						
Stage of Orifice Controld (#)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)							
Orifice Area (sq. inches)															
User Input: Vertical Orifice (Circular or Rectange	<u>ılar)</u>		Ì				Calculated Parame	ters for Vertical Orit	fice						
Invert of Vertical Orifice -	Not Selected	Not Selected	ft (rolativo to bacin	bottom at Stago -	0 ft) Vor	tical Orifica Aroa -	Not Selected	Not Selected	n 2						
Depth at top of Zone using Vertical Orlife =	N/A	N/A N/A	ft (relative to basin	i bottom at Stage =	0 ft) Vertica	I Orifice Centroid =	N/A	N/A N/A	feet						
Vertical Orifice Diameter =	N/A	N/A	inches	y-				.,							
User Input: Overflow Weir (Dropbox with Flat or	Zone 3 Weir	Not Selected	angular/ I rapezoida	al Weir and No Outl	<u>et Pipe)</u>		Zono 2 Woir	Not Selected	eir						
Overflow Weir Front Edge Height, Ho =	1.70	N/A	Gh (and a bina has been in the				ZUIIE 3 WEII	NUL SEIELLEU	Zone 3 Weir Not Selected Zone 3 Weir Not Selected						
		IN/A	It (relative to basin t	oottom at Stage = 0 f	t) Height of Grat	e Upper Edge, Ht =	2.41	N/A	feet						
Overflow weir Front Edge Length =	2.92	N/A N/A	feet	oottom at Stage = 0 t	t) Height of Grat Overflow W	e Upper Edge, H _t = /eir Slope Length =	2.41 2.92	N/A N/A	feet feet						
Overflow Weir Front Edge Length = Overflow Weir Grate Slope =	2.92 4.00	N/A N/A N/A	feet H:V	oottom at Stage = 0 t Gi	t) Height of Grat Overflow W rate Open Area / 10	e Upper Edge, $H_t =$ /eir Slope Length = 10-yr Orifice Area =	2.41 2.92 9.51	N/A N/A N/A	feet feet						
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Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = User Input: Emergency Spillway (Rectangular or Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) = Maximum Ponding Depth (re)	2.92 4.00 2.83 Type C Grate 50% Zone 3 Restrictor 0.25 18.00 6.90 Trapezoidal) 2.70 10.00 0.00 1.00 <i>Trapezoidal</i>) 2.70 10.00 0.00 1.00 <i>Trapezoidal</i>) 2.70 10.00 0.00 1.00 <i>Trapezoidal</i>) 2.70 10.00 0.00 1.00 <i>N/A</i> N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	N/A	If (relative to basin to feet H:V feet H:V feet % ectangular Orifice) ft (distance below basin to inches inches inches bottom at Stage = 4P hydrographs and 2 Year 0.79 0.141 0.141 0.141 0.141 0.141 0.141 0.141 0.141 0.151 5.6 N/A N/A N/A 51 53 1.13 0.10	xottom at Stage = 0 1 Gi O O (asin bottom at Stage Half-Cen 0 ft) 1.07 0.202 0.202 0.202 0.202 0.2 0.2 0.2 0.2	t) Height of Grat Overflow V ate Open Area / 10 verflow Grate Open Verflow Grate Open Verflow Grate Open Deflow Grate Open Car a Angle of Restrict Spillway D Stage at Basin Area at Basin Area at Basin Area at Basin Area at Car Basin Area at Basin Area at Car Basin Area at Car Car Basin Area at Car Basin Area at Car Car Car Basin Area at Car Car Car Car Car Car Car Car Car Car	e Upper Edge, H _t = eleir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/o Debris = elculated Parameter utlet Orifice Area = t Orifice Centroid = tor Plate on Pipe = esign Flow Depth= Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Fop of Freeboard = Cop	2.41 2.92 9.51 5.93 2.96 2.96 2.96 2.96 2.062 0.62 0.34 1.34 <u>Calculated Parame</u> 0.52 4.22 0.33 0.94 2.23 0.94 2.23 0.491 0.491 0.491 0.491 0.491 0.491 0.491 0.491 0.491 0.491 0.491 0.5 0.0491 0.5 0.0491 0.5 0.62 0.73 0.23 0.74 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	N/A N/A N/A N/A N/A N/A NA NA NA NA N/A 100 Year 2.69 0.609 0.609 4.7 1.59 11.3 3.1 0.7 Overflow Weir 1 0.5 N/A 65 73 2.46 0.25	feet feet feet ft ² ft ² feet radians 500 Year 3.98 0.935 0.9370 0.9370 0.9370 0.93700000000000000000000000000000000000						

DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

	Inflow Hydrog	rapns								
	The user can ov	verride the calcu	lated inflow hyd	lrographs from t	his workbook w	ith inflow hydro	graphs develope	ed in a separate p	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5100 1111	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.05	1.92
	0:20:00	0.00	0.00	1 10	1.63	2.13	1.61	2 10	2.51	4.10
	0.25.00	0.00	0.00	2.41	3.49	4.66	3 51	4 56	5 30	9.66
	0:20:00	0.00	0.00	2.41	3.70	4.83	7.06	9.02	10.83	16.53
	0:35:00	0.00	0.00	2.05	3.10	4.01	7.06	8 94	11 35	17 20
	0:40:00	0.00	0.00	1.87	2.52	3.26	6.30	7.94	9,99	15.10
	0:45:00	0.00	0.00	1.45	2.02	2.65	5.17	6.52	8.51	12.84
	0:50:00	0.00	0.00	1.19	1.71	2.19	4.35	5.47	7.06	10.66
	0:55:00	0.00	0.00	1.00	1.42	1.84	3.49	4.40	5.86	8.85
	1:00:00	0.00	0.00	0.82	1.17	1.53	2.85	3.60	4.98	7.52
	1:05:00	0.00	0.00	0.69	0.97	1.29	2.34	2.96	4.25	6.41
	1:10:00	0.00	0.00	0.55	0.87	1.18	1.79	2.27	3.10	4.71
	1:15:00	0.00	0.00	0.48	0.79	1.15	1.49	1.90	2.42	3.71
	1:20:00	0.00	0.00	0.44	0.71	1.04	1.23	1.56	1.81	2.78
	1:25:00	0.00	0.00	0.42	0.66	0.90	1.06	1.35	1.42	2.19
	1:30:00	0.00	0.00	0.41	0.63	0.81	0.90	1.14	1.18	1.84
	1:35:00	0.00	0.00	0.40	0.61	0.74	0.79	1.00	1.02	1.59
	1:40:00	0.00	0.00	0.39	0.53	0.70	0.72	0.91	0.92	1.44
	1:45:00	0.00	0.00	0.39	0.48	0.67	0.68	0.85	0.86	1.34
	1:50:00	0.00	0.00	0.39	0.45	0.65	0.65	0.82	0.83	1.30
	1:55:00	0.00	0.00	0.32	0.42	0.61	0.63	0.80	0.82	1.28
	2:00:00	0.00	0.00	0.28	0.39	0.55	0.63	0.79	0.82	1.28
	2:05:00	0.00	0.00	0.18	0.26	0.36	0.41	0.52	0.54	0.85
	2:10:00	0.00	0.00	0.12	0.17	0.24	0.27	0.34	0.36	0.56
	2:15:00	0.00	0.00	0.08	0.11	0.15	0.17	0.22	0.23	0.36
	2:20:00	0.00	0.00	0.04	0.06	0.09	0.11	0.14	0.14	0.22
	2:25:00	0.00	0.00	0.03	0.04	0.05	0.07	0.08	0.09	0.13
	2:30:00	0.00	0.00	0.01	0.02	0.03	0.03	0.04	0.05	0.07
	2:35:00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03
	2:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.15.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3.25.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5.55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stago - Storago	Stage	Area	Area	Volume	Volume	Total	I
Description		2-		3-		Outflow	
· · · · ·	[π]	[ft ⁻]	[acres]	[ft*]	[ac-π]	[crs]	
							For best results, include the
							stages of all grade slope
	1						changes (e.g. ISV and Floor
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of a
							outlets (e.g. vertical orifice,
							overflow grate, and spillway
							where applicable).
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Attachment D: CO 119 RTD Park-n-Ride Drainage Report

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)

Project: SH119 BRT - 63rd Street Station PnR

Basin ID:	RTD PnR Or	nsite Full Spectrum Detention Bas	in (63-PR1 thru 63-F	PR5)								
ZONE 3	Conte a	-										
100-711	T	T										
account annot moch	1	5			-							
E ZOHE	AND	CONFICE	Depth Increment =		ft							
PERMANENT ORPO	as Configure	tion (Potention Dand)	Stage - Storage	Stage	Optional	Length	Width	Area	Override	Area	Volume	Volume
Example 2016	comgura	ation (Retention Pond)	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)
Watershed Information			Top of Micropool		0.00			-	0	0.000		
Selected BMP Type =	EDB	1			0.50				5,713	0.131	1,428	0.033
Watershed Area =	3.52	acres	-		1.00			-	11.156	0.256	5.645	0.130
Watershed Length =	596	ft	-		1.50				12,100	0.278	11.459	0.263
Watershed Length to Centroid =	279	ft	-		2.00				12,946	0.297	17,721	0.407
Watershed Slope =	0.015	ft/ft			2.50				13.816	0.317	24,411	0.560
Watershed Imperviousness =	72.80%	percent			3.00	-		-	14,712	0.338	31,543	0.724
Percentage Hydrologic Soil Group A =	0.0%	percent			3.50				15.633	0.359	39,129	0.898
Percentage Hydrologic Soil Group B =	0.0%	percent	-		4.00				16,580	0.381	47,183	1.083
Percentage Hydrologic Soil Groups C/D =	100.0%	percent			4.50				17,552	0.403	55,716	1.279
Target WQCV Drain Time =	40.0	hours										
Location for 1-hr Rainfall Depths =	User Input											
After providing required inputs above inc	ludina 1-hour	rainfall										
depths, click 'Run CUHP' to generate rund	off hydrograph	hs using						-				
the embedded Colorado Urban Hydro	graph Proced	lure. Optional User Overrides										
Water Quality Capture Volume (WQCV) =	0.084	acre-feet acre-feet										
Excess Urban Runoff Volume (EURV) =	0.250	acre-feet acre-feet						-				
2-yr Runoff Volume (P1 = 0.79 in.) =	0.148	acre-feet 0.79 inches		-				-				
5-yr Runoff Volume (P1 = 1.06 in.) =	0.215	acre-feet 1.06 inches										
10-yr Runoff Volume (P1 = 1.33 in.) =	0.288	acre-feet 1.33 inches						-				
25-yr Runoff Volume (P1 = 1.78 in.) =	0.425	acre-feet 1.78 inches						-				
50-yr Runoff Volume (P1 = 2.17 in.) =	0.541	acre-feet 2.17 inches				-		-				
100-yr Runoff Volume (P1 = 2.61 in.) =	0.677	acre-feet 2.61 inches						-				
500-yr Runoff Volume (P1 = 3.82 in.) =	1.040	acre-feet 3.82 inches						-				
Approximate 2-yr Detention Volume =	0.148	acre-feet				-		-				
Approximate 5-yr Detention Volume =	0.220	acre-feet										
Approximate 10-yr Detention Volume =	0.272	acre-feet				-		-				
Approximate 25-yr Detention Volume =	0.338	acre-feet				-		-				
Approximate 50-yr Detention Volume =	0.376	acre-feet										
Approximate 100-yr Detention Volume =	0.433	acre-feet										
								-				
Define Zones and Basin Geometry		7										
Zone 1 Volume (WQCV) =	0.084	acre-feet										
Zone 2 Volume (EURV - Zone 1) =	0.165	acre-feet						-				
Zone 3 Volume (100-year - Zones 1 & 2) =	0.183	acre-feet						-				
Total Detention Basin Volume =	0.433	acre-feet										
Initial Surcharge Volume (ISV) =	user	ft ³						-				
Initial Surcharge Depth (ISD) =	user	ft				-						
Total Available Detention Depth (H _{total}) =	user	ft										
Depth of Trickle Channel (H_{TC}) =	user	ft										
Slope of Trickle Channel (S _{TC}) =	user	ft/ft						-				
Slopes of Main Basin Sides (Smain) =	user	H:V						-				
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	_										
Tribial Complement Area (A) -												
Initial Surcharge Area (A _{SV}) =	user					-		-				
Surcharge Volume Lenguri (L _{ISV}) =	user					-		-				
Depth of Basin Floor (Herees) =	user	n. #	-			-						
Length of Basin Floor (Lenge) =	user		-					-				
Width of Basin Floor (Wei ees) =	user	n. #	-			-						
Area of Basin Floor (Aricon) =	user	ft ²	-					-				
Volume of Basin Floor (Vr) =	user	ft 3				-		-				
Depth of Main Basin (Herea) =	user	ft.				-		-				
Length of Main Basin (LMAIN) =	user	ft				-		-				
Width of Main Basin (W _{MATH}) =	user	ft										
Area of Main Basin (Aman) =	user	ft ²										
Volume of Main Basin (V _{MAIN}) =	user	ft ³										
Calculated Total Basin Volume (Vtntal) =	user	acre-feet										
		-										
					-	-						
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MHFD-Detention, Version 4.05 (January 2022)

DETENTION BASIN OUTLET STRUCTURE DESIGN										
MHFD-Detention, Version 4.05 (January 2022)										
Project: Basin ID:	SH119 BRT - 63rd RTD PnR Onsite Fi	Street Station Pne III Spectrum Deten	tion Basin (63-PR1	thru 63-PR5)						
ZONE 3				Estimated	Estimated					
		-		Stage (ft)	Volume (ac-ft)	Outlet Type				
VOLUME, EURY WOCV		-	Zone 1 (WQCV)	0.81	0.084	Orifice Plate]			
	100-YEAR		Zone 2 (EURV)	1.46	0.165	Orifice Plate				
PERMANENT ORIFICES	OniFice		Zone 3 (100-year)	2.09	0.183	Weir&Pipe (Restrict)				
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	0.433		1			
User Input: Orifice at Underdrain Outlet (typically	y used to drain WQC	CV in a Filtration BM	<u>4P)</u>			I	Calculated Parame	ters for Underdrain		
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underd	Irain Orifice Area =	N/A	ft²		
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet		
	The second second							,		
User Input: Orifice Plate with one or more orifice	es or Elliptical Slot v	Veir (typically used	to drain WQCV and	/or EURV in a seair	nentation BMP) WO Orifi	- Aron por Pow -	Calculated Parame	ters for Plate		
Denth at top of Zone using Orifice Plate =	1.46	IT (relative to basin	bottom at Stage =	0 TC) 0 ft)	WQ Onin Fili	ce area per now -	7.292E-05 Ν/Δ	ft- foot		
Orifice Plate: Orifice Vertical Spacing =	8.00	inches	Douom at Stage	010	Ellipti	ical Slot Centroid =	N/A	feet		
Orifice Plate: Orifice Area per Row =	1.05	inches (diametr	er = 1-1/8 inches)		E	llintical Slot Area =	N/A	ft ²		
		54	u, ,			inpeter etc.				
User Input: Stage and Total Area of Each Orifice	Row (numbered fr	om lowest to highe	<u>st)</u>							
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)		
Stage of Orifice Centroid (ft)	0.00	0.70	1.40							
Orifice Area (sq. inches)	1.05	1.05	1.05							
									I	
Channel (Channel)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)		
Stage of Urifice Lentroid (IT)										
Office Area (Sq. incres)										
User Input: Vertical Orifice (Circular or Rectange	ular)						Calculated Parame	ters for Vertical Orif	ice	
	Not Selected	Not Selected					Not Selected	Not Selected		
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ver	tical Orifice Area =	N/A	N/A	ft ²	
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertical	Orifice Centroid =	N/A	N/A	feet	
Vertical Orifice Diameter =	N/A	N/A	inches							
						-				
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and C	Jutlet Pipe OR Rect	angular/Trapezoida	Weir and No Outle	et Pipe)		Calculated Parame	ters for Overflow W	eir	
User Input: Overflow Weir (Dropbox with Flat or	Zone 3 Weir	Outlet Pipe OR Rect Not Selected	tangular/Trapezoida	I Weir and No Outle	<u>et Pipe)</u>		Calculated Parame	ters for Overflow W Not Selected	eir	
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho =	r Sloped Grate and C Zone 3 Weir 1.50	Dutlet Pipe OR Rect Not Selected N/A	tangular/Trapezoida	<u>I Weir and No Outle</u> ottom at Stage = 0 f	et Pipe) t) Height of Grate	e Upper Edge, H _t =	Calculated Parame Zone 3 Weir 2.21	ters for Overflow W Not Selected N/A	eir feet	
User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	r <u>Sloped Grate and C</u> Zone 3 Weir 1.50 2.92	Dutlet Pipe OR Rect Not Selected N/A N/A	tangular/Trapezoida ft (relative to basin b feet	<u>I Weir and No Outle</u> nottom at Stage = 0 f	t) Height of Grate Overflow W	e Upper Edge, H _t = 'eir Slope Length =	Calculated Parame Zone 3 Weir 2.21 2.92 9 51	ters for Overflow W Not Selected N/A N/A	<u>eir</u> feet feet	
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User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =	Sloped Grate and (Zone 3 Weir 1.50 2.92 4.00 2.83 Type C Grate	Outlet Pipe OR Rect Not Selected N/A N/A N/A N/A N/A	tangular/Trapezoida ft (relative to basin t feet H:V feet	ll Weir and No Outle Rottom at Stage = 0 f Gr Ov C	et Pipe) t) Height of Grate Overflow W ate Open Area / 10 verflow Grate Open Vverflow Grate Open	e Upper Edge, H _t = /eir Slope Length = 0-yr Orifice Area = Area w/o Debris =	Calculated Parame Zone 3 Weir 2.21 2.92 8.51 5.93 2.96	ters for Overflow W Not Selected N/A N/A N/A N/A N/A	<u>eir</u> feet feet ft ² ft ²	
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User Input: Overflow Weir (Dropbox with Flat or Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	r Sloped Grate and 1 Zone 3 Weir 1.50 2.92 4.00 2.83 Type C Grate 50% (Circular Orifice, Re Zone 3 Restrictor 0.25 18.00	Dutlet Pipe OR Rect N/A N/A N/A N/A N/A N/A N/A Strictor Plate, or R/ Not Selected N/A N/A	tangular/Trapezoida ft (relative to basin t feet H:V feet % ectangular Orifice) ft (distance below ba inches	Il Weir and No Outli bottom at Stage = 0 f Gr On C Isin bottom at Stage -	t) Height of Grate Overflow W ate Open Area / 10 /erflow Grate Open Jverflow Grate Open <u>Ca</u> = 0 ft) Ot Outlet	e Upper Edge, H _t = leir Slope Length = 0-yr Orifice Area = Area w/o Debris = n Area w/ Debris = lculated Parameter: Jtlet Orifice Area = : Orifice Centroid =	Calculated Parame Zone 3 Weir 2.21 2.92 8.51 5.93 2.96 s for Outlet Pipe w/ Zone 3 Restrictor 0.70 0.36	ters for Overflow W Not Selected N/A N/A N/A N/A N/A Flow Restriction Pla Not Selected N/A N/A	eir feet feet ft ² ft ² ate ft ² fteet	
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DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

	Inflow Hydrog	raphs								
	The user can ov	verride the calcu	lated inflow hyd	lrographs from t	this workbook w	ith inflow hydro	graphs develope	ed in a separate p	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
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	0.10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.10.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.03	0.38
	0.13.00	0.00	0.00	0.09	0.38	0.61	0.53	0.80	0.88	1.54
	0.20.00	0.00	0.00	0.96	2.17	1.00	2.16	1.04	2.10	3.59
	0.23.00	0.00	0.00	2.14	3.17	4.30	5.10	9.75	4.90	0.17
	0.30.00	0.00	0.00	2.49	3.30	4.70	0.82	0.16	11.64	17.66
	0:35:00	0.00	0.00	1.96	2 70	3.57	6.73	9.10	10.70	16.10
	0:45:00	0.00	0.00	1.50	2.70	3.01	5.80	7 32	9.52	14.38
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	0:55:00	0.00	0.00	1.52	1.52	2.30	4 14	5.22	6.94	10.48
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	1:15:00	0.00	0.00	0.58	0.91	1.17	2.10	2 54	3 33	5.08
	1:20:00	0.00	0.00	0.50	0.79	1.55	1 54	1.95	2 41	3.69
	1:25:00	0.00	0.00	0.30	0.73	0.99	1.34	1.55	1.83	2.83
	1:30:00	0.00	0.00	0.44	0.68	0.55	1.05	1 34	1.05	2.05
	1:35:00	0.00	0.00	0.43	0.65	0.05	0.91	1 15	1.77	1.95
	1:40:00	0.00	0.00	0.43	0.58	0.01	0.91	1.03	1.25	1.55
	1:45:00	0.00	0.00	0.41	0.53	0.72	0.75	0.95	0.98	1.54
	1:50:00	0,00	0.00	0.41	0.49	0,70	0,71	0.89	0.91	1.43
	1:55:00	0.00	0.00	0.35	0.46	0.66	0.68	0.85	0.86	1.36
	2:00:00	0.00	0.00	0.31	0.43	0.59	0.66	0.83	0.84	1.30
	2:05:00	0.00	0.00	0.22	0.15	0.42	0.00	0.59	0.60	0.95
	2:10:00	0.00	0.00	0.22	0.22	0.30	0.33	0.42	0.00	0.68
	2:15:00	0.00	0.00	0.10	0.15	0.30	0.23	0.12	0.15	0.48
	2:20:00	0.00	0.00	0.07	0.10	0.14	0.16	0.20	0.21	0.32
	2:25:00	0.00	0.00	0.05	0.07	0.09	0.11	0.13	0.14	0.21
	2:30:00	0.00	0.00	0.03	0.04	0.06	0.07	0.09	0.09	0.14
	2:35:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.09
	2:40:00	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.03	0.04
	2:45:00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01
	2:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.05 (January 2022)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stago - Storago	Stage	Area	Area	Volume	Volume	Total	I
Description		2-		3-		Outflow	
· · · · ·	[π]	[ft ⁻]	[acres]	[ft*]	[ac-π]	[crs]	
							For best results, include the
							stages of all grade slope
	1						changes (e.g. ISV and Floor
							from the S-A-V table on
							Sheet 'Basin'.
							Also include the inverts of a
							outlets (e.g. vertical orifice,
							overflow grate, and spillway
							where applicable).
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APPENDIX G

STORM DRAIN SYSTEM CALCULATIONS

NIWOT ROAD P-n-R STORM DRAIN SYSTEM DESIGN FLOW RATES FINAL DEVELOPED HYDROLOGIC CONDITIONS

Storm Drain Inlets

Contributing Basins to SD Inlet	SD Inlet ID	Computed Q100 (cfs)	Inlet Capacity (cfs)	Proposed Inlet	Comments
NW-PR1 (Sump)	IN 1	3.4	5.4	5' Type R Inlet	Max Depth = 6 inches
NW-PR2 (Sump)	IN 2	3.7	5.4	5' Type R Inlet	Max Depth = 6 inches
NW-PR3 (Sump)	IN 3	6.3	8.3	10' Type R Inlet	Max Depth = 6 inches
NW-PR4 (Sump)	IN 4	3.4	5.4	5' Type R Inlet	Max Depth = 6 inches
NW-PR7 (Continuous)	IN 5	3.9	3.8	10' Type R Inlet	99% Capture

Storm Drain Pipes

Contributing Basins to SD Pipe	Upstream Node	Downstream Node	Computed Q100 (cfs)	Length (ft)	Slope (ft/ft)	Pipe Size (inch)*	Comments
NW-PR6	FES1	MH1	3.1	55.0	0.027	18 inch RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
18" RCP under Niwot, NW-PR6	MH1	MH2, MH3	16.6	362.0	0.004	30 inch RCP	30" RCP @ 0.4% FF Cap = 25.9 cfs
18" RCP under Niwot, NW-PR6, DB Outflow	MH3	FES2	21.0	25.0	0.008	30 inch RCP	30" RCP @ 0.4% FF Cap = 25.9 cfs
NW-PR2	IN2	IN1	3.7	150.0	0.005	18 inch RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
NW-PR4	IN4	IN1	3.4	85.0	0.005	18 inch RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
NW-PR1, NW-PR2, NW-PR4	IN1	DB	10.5	15.0	0.013	24 inch RCP	24" RCP @ 0.5% FF Cap = 16 cfs
NW-PR7	IN5	MH-O	3.9	10.0	0.005	18 inch RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
NW-PR3	IN3	DB	6.3	90.0	0.003	24 inch RCP	24" RCP @ 0.3% FF Cap = 12 cfs

* Pipe culvert size approximated based on Bently Flowmaster normal depth flowing-full (FF) capacity

18" RCP under Niwot	Length (ft)	H(ft)	Slope (ft/ft)	Q full (cfs)
Existing culvert under Niwot Road	136	2.17	0.016	13.5

63rd Street P-n-R

STORM DRAIN SYSTEM DESIGN PROPOSED HYDROLOGIC CONDITIONS

Storm Drain Inlets

Contributing Basins to SD Inlet	SD Inlet ID	Computed Q100 (cfs)	Inlet Capacity (cfs)	Proposed Inlet	Comments
63-PR1 (Sump)	IN 1	3.6	5.4	5' Type R Inlet	Max Depth = 6 inches
63-PR2 (Sump)	IN 2	3.7	5.4	5' Type R Inlet	Max Depth = 6 inches
63-PR3 (Sump)	IN 3	4.3	5.4	5' Type R Inlet	Max Depth = 6 inches
63-PR4 (Area Inlet)	IN 4	7.3	8.3	CDOT Type C	
63-PR6 (Continuous)	IN 5	3.7	4.0	10' Type R Inlet	99% Capture
63-PR8 (Sump)	IN 6	2.5	5.4	5' Type R Inlet	Max Depth = 6 inches
63-PR7*	IN 7	5.8			

* For SD Inlet and pipe design for Basin 63-PR7, refer to CO 119 Safety and Mobility Improvements Project, Preliminary Drainage Report, August 2022.

Storm Drain Pipes

Contributing Desire to CD Dine	Linetroom Node	Downstream	Computed	Longth (ft)		Dine Size (inch)*	Commente
Contributing Basins to SD Pipe	Opstream Node	Node	Q100 (cfs)	Length (It)	Slope (It/It)	Pipe Size (inch)*	Comments
offsite CDOT Median Area (Muller Basin P172C**)	FES 1	MH 1	11.9	75.0	0.005	24" RCP	24" RCP @ 0.5% FF Cap = 16 cfs
DB Outflow	DB Out	MH 1	3.1	30.0	0.005	18" RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
P172C, DB Outflow	MH 1	MH 2	15.0	207.0	0.005	24" RCP	24" RCP @ 0.5% FF Cap = 16 cfs
63-PR8	IN 6	MH 2	2.5	35.0	0.086	18" RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
P172C, DB Outflow, 63-PR8	MH 2	CBC	17.5	28.0	0.005	30" RCP	30" RCP @ 0.4% FF Cap = 25.9 cfs
63-PR3	IN 3	IN 2	4.3	45.0	0.005	18" RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
63-PR3, 63-PR2	IN 2	IN 1	8.0	95.0	0.005	24" RCP	24" RCP @ 0.5% FF Cap = 16 cfs
63-PR4	IN 4	IN 1	7.3	55.0	0.005	18" RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs
63-PR1, 63-PR2, 63-PR3, 63-PR4	IN 1	DB In	18.9	35.0	0.005	30" RCP	30" RCP @ 0.4% FF Cap = 25.9 cfs
63-PR6	IN 5	CBC	3.7	230.0	0.022	18" RCP	18" RCP @ 0.5% FF Cap = 7.4 cfs

* Pipe culvert size approximated based on Bently Flowmaster normal depth flowing-full (FF) capacity

** Basin P172C - refer to CO 119 Safety and Mobility Improvements Project, Preliminary Drainage Report, August 2022.

Design Information (Input)	MINOR MAJOR			
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.0	inches
Grate Information		MINOR	MAJOR	C Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	_
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
I ow Head Performance Reduction (Calculated)		MINOR	MAIOR	
Depth for Grate Midwidth	d	MINOR N/A	M/A	ft
Depth for Curb Opening Weir Equation	d _{Grate} –	0.33	0.33	ft
Combination Inlet Performance Peduction Eactor for Long Inlets		0.55	0.55	10
Curb Opening Performance Reduction Factor for Long Inlets	PEa -	1.00	1.00	-
Grated Inlet Performance Reduction Factor for Long Inlets	RE _{curb} =	N/A	N/A	-
oraced fineer enormance reduction ractor for Eorig fillets	Grate -	in/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.0	4.0	cfs

Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_o(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.33	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{combination} =	0.57	0.57	
Curb Opening Performance Reduction Factor for Long Inlets	$RF_{Curb} =$	0.93	0.93	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
				_
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.3	8.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.0	8.0	cfs



Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Typ	e C Grate	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	8.00	8.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	7.8	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	2.92	2.92	feet
Width of a Unit Grate	W _o =	2.92	2.92	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	0.70	0.70	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	0.50	0.50	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_w (G) =	2.41	2.41	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	0.67	0.67	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	N/A	N/A	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	N/A	N/A	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	N/A	N/A	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	N/A	N/A	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	N/A	N/A	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	N/A	N/A	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	N/A	N/A	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	N/A	N/A	
l ow Head Performance Reduction (Calculated)		MINOR	MAIOR	
Depth for Grate Midwidth	d _{crata} =	0.802	0.954	ft
Depth for Curb Opening Weir Equation	d _{curb} =	N/A	N/A	ft
Combination Inlet Performance Reduction Eactor for Long Inlets	RF _{combination} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RFcurb =	N/A	N/A	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	0.95	1.00	
5				-
	_	MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a =$	6.0	8.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	$Q_{PEAK REQUIRED} =$	4.0	8.0	cfs

Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
	0.012	
	0.015	£/A
Channel Slope	0.01800	10/11
Normal Depth	1.50	1L #
Diameter	1.50	it
Results		
Discharge	13.29	ft³/s
Flow Area	1.77	ft²
Wetted Perimeter	4.71	ft
Hydraulic Radius	0.38	ft
Top Width	0.00	ft
Critical Depth	1.36	ft
Percent Full	100.0	%
Critical Slope	0.01400	ft/ft
Velocity	7.52	ft/s
Velocity Head	0.88	ft
Specific Energy	2.38	ft
Froude Number	0.00	
Maximum Discharge	14.29	ft³/s
Discharge Full	13.29	ft³/s
Slope Full	0.01600	ft/ft
Flow Type	SubCritical	
GVF Input Data		
Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	100 00	%
Downstream Velocity	Infinity	ft/s

Worksheet for 18 inch under Niwot

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Worksheet for 18 inch under Niwot

GVF Output Data		
Upstream Velocity	Infinity	ft/s
Normal Depth	1.50	ft
Critical Depth	1.36	ft
Channel Slope	0.01600	ft/ft
Critical Slope	0.01400	ft/ft

Project Description				
Friction Method	Manning Formula			
Solve For	Discharge			
Input Data				
, Deventues of Oceafficient		0.012		
Roughness Coefficient		0.013	£4/£4	
		1.50	11/11 A	
		1.50	п #	
Diameter		1.50	п	
Results				
Discharge		7.43	ft³/s	
Flow Area		1.77	ft²	
Wetted Perimeter		4.71	ft	
Hydraulic Radius		0.38	ft	
Top Width		0.00	ft	
Critical Depth		1.06	ft	
Percent Full		100.0	%	
Critical Slope		0.00703	ft/ft	
Velocity		4.20	ft/s	
Velocity Head		0.27	ft	
Specific Energy		1.77	ft	
Froude Number		0.00		
Maximum Discharge		7.99	ft³/s	
Discharge Full		7.43	ft³/s	
Slope Full		0.00500	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Lenath		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		100.00	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for 18 inch RCP 0.5 Percent Slope

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Worksheet for 18 inch RCP 0.5 Percent Slope

Upstream Velocity	Infinity	ft/s
Normal Depth	1.50	ft
Critical Depth	1.06	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.00703	ft/ft

Project Description					
Friction Method	Manning Formula				
Solve For	Discharge				
Input Data					
Roughness Coefficient		0.013			
Channel Slope		0.00500	ft/ft		
Normal Depth		2.00	ft		
Diameter		2.00	ft		
Results					
Discharge		16.00	ft³/s		
Flow Area		3.14	ft²		
Wetted Perimeter		6.28	ft		
Hydraulic Radius		0.50	ft		
Top Width		0.00	ft		
Critical Depth		1.44	ft		
Percent Full		100.0	%		
Critical Slope		0.00662	ft/ft		
Velocity		5.09	ft/s		
Velocity Head		0.40	ft		
Specific Energy		2.40	ft		
Froude Number		0.00			
Maximum Discharge		17.21	ft³/s		
Discharge Full		16.00	ft³/s		
Slope Full		0.00500	ft/ft		
Flow Type	SubCritical				
GVF Input Data					
Downstream Depth		0.00	ft		
Length		0.00	ft		
Number Of Steps		0			
GVF Output Data					
Upstream Depth		0.00	ft		
Profile Description					
Profile Headloss		0.00	ft		
Average End Depth Over Rise		0.00	%		
Normal Depth Over Rise		100.00	%		
Downstream Velocity		Infinity	ft/s		

Worksheet for 24 inch RCP 0.5 Percent Slope

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Worksheet for 24 inch RCP 0.5 Percent Slope

Upstream Velocity	Infinity	ft/s
Normal Depth	2.00	ft
Critical Depth	1.44	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.00662	ft/ft

Project Description				
Friction Method	Manning Formula			
Solve For	Discharge			
Input Data				
Paurahanana Calaffiniant		0.012		
Channel Slope		0.013	ft/ft	
		0.00300	11/11 #	
Diameter		2.00	ft	
Reculte				
results				
Discharge		12.39	ft³/s	
Flow Area		3.14	ft²	
Wetted Perimeter		6.28	ft	
Hydraulic Radius		0.50	ft	
Top Width		0.00	ft	
Critical Depth		1.27	ft	
Percent Full		100.0	%	
Critical Slope		0.00567	ft/ft	
Velocity		3.94	ft/s	
Velocity Head		0.24	ft	
Specific Energy		2.24	ft	
Froude Number		0.00		
Maximum Discharge		13.33	ft³/s	
Discharge Full		12.39	ft³/s	
Slope Full		0.00300	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		100.00	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for 24 inch RCP 0.3 percent Slope

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Worksheet for 24 inch RCP 0.3 percent Slope

Upstream Velocity	Infinity	ft/s
Normal Depth	2.00	ft
Critical Depth	1.27	ft
Channel Slope	0.00300	ft/ft
Critical Slope	0.00567	ft/ft

Project Description				
Friction Method	Manning Formula			
Solve For	Discharge			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00400	ft/ft	
Normal Depth		2.50	ft	
Diameter		2.50	ft	
Results				
Discharge		25.94	ft³/s	
Flow Area		4.91	ft²	
Wetted Perimeter		7.85	ft	
Hydraulic Radius		0.63	ft	
Top Width		0.00	ft	
Critical Depth		1.74	ft	
Percent Full		100.0	%	
Critical Slope		0.00583	ft/ft	
Velocity		5.28	ft/s	
Velocity Head		0.43	ft	
Specific Energy		2.93	ft	
Froude Number		0.00		
Maximum Discharge		27.90	ft³/s	
Discharge Full		25.94	ft³/s	
Slope Full		0.00400	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		100.00	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for 30 inch RCP 0.4 Percent Slope

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Worksheet for 30 inch RCP 0.4 Percent Slope

Upstream Velocity	Infinity	ft/s
Normal Depth	2.50	ft
Critical Depth	1.74	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.00583	ft/ft

APPENDIX H

FIR DRAINAGE PLANS



